



5th International Conference
"Advanced Composite Materials Engineering"
COMAT 2014
16-17 October 2014, Braşov, Romania

ASPECTS ON STRUCTURAL SCATLINGS OF SMALL CRAFTS BUILD FROM COMPOSITE MATERIALS

Ionel Chirică, Professor, NA, PhD.¹, Dumitru Lupaşcu, Naval Architect²

¹University "Dunărea de Jos" - Galaţi;

²Romanian Naval Authority

Abstract: *Development and improvement of manufacturing technologies for composite materials with more and more improved characteristics, resulted in use of these materials in shipbuilding as well, and particularly in boatbuilding. Scantling calculations of strength structures for these boats are carried out based on the Rules of Classification Societies for ships and recently according to ISO 12215 series of standards. In this article, are presented results of such scantling calculations of structural elements of one leisure boat, based on relevant standard, using CraftSoft software. This software, developed by authors in EXCEL, can calculate the required scantling structural properties for boats constructed of aluminum alloys, steel, wood and fiber reinforced plastic, single skin and sandwich laminates, according to ISO 12215-5 standard.*

Keywords: *composite material, small craft, scantling*

1. INTRODUCTION

Traditional materials used in shipbuilding are steel and aluminum, but due to development and improvement of manufacturing technologies for composite materials with improved characteristics, these materials commenced to replace more and more the traditional ones as a consequence of their advantages: low density, high endurance to mechanical actions, corrosion and fatigue resistance, high capacity to attenuate vibrations, special magnetic properties, low energy consumption and lower cost installations for manufacturing.

But usage of composite materials, due to lower mechanical properties in comparison with metals, is limited to construction of small and medium ships, up to 70 meters and construction of some structures onboard large ships where effective stresses do not reach big values, e.g. superstructures or their inner bulkheads, or other fittings or arrangements onboard.

The most used composite materials for building small ships are those fibre glass reinforced and those of sandwich type whose characteristics are prescribed by following standards:

1. ISO 12215-1: 2003 Small craft. Hull construction and scantlings. Part 1: Materials: Thermosetting resins, glass fibre reinforcement, reference laminate;
2. ISO 12215-2: 2003 Small craft. Hull construction and scantlings. Part 2 : Materials: Core materials for sandwich construction, embedded materials,

as well as by the Rules of some classification societies for ships, e.g. Lloyd's Register (LR), American Bureau of Shipping (ABS), DNV –GL, Bureau Veritas (BV), etc.

Recently, in the construction of ship's strength structures, the unrestricted use of a new combination of materials based on SPS (sandwich plate system) concept have commenced, materialized in steel sandwich panels which consists of three layers: two external layers of steel and one internal core layer, see figure 1.

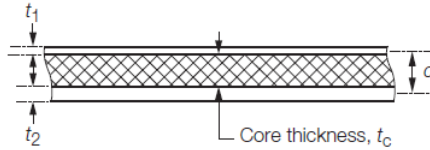


Figure 1: Steel sandwich panel

Regulations for fabrication, characteristics and scantling of this new composite material could be found at some classification societies as LR, DNV-GL, etc.

2. SCANTLING OF HULLS BUILT IN COMPOSITE MATERIALS

Boats are small crafts with length less than 24 meters, with broad scope of use, from performing commercial services to leisure or sport activities. Scantling of those boats, built in composite materials, is done based on Rules of classification societies, but now, this scantling could be done as well according to following recent standards:

1. ISO 12215-5: 2008 Small craft. Hull construction and scantlings. Part 5: Design pressures for monohulls, design stresses, scantlings determination;
2. ISO 12215-6: 2008 Small craft. Hull construction and scantlings. Part 6 : Structural arrangements and details.

In principle, scantling of structural elements of boats based on these regulations is carried out according to a general scheme indicated in figure 2:

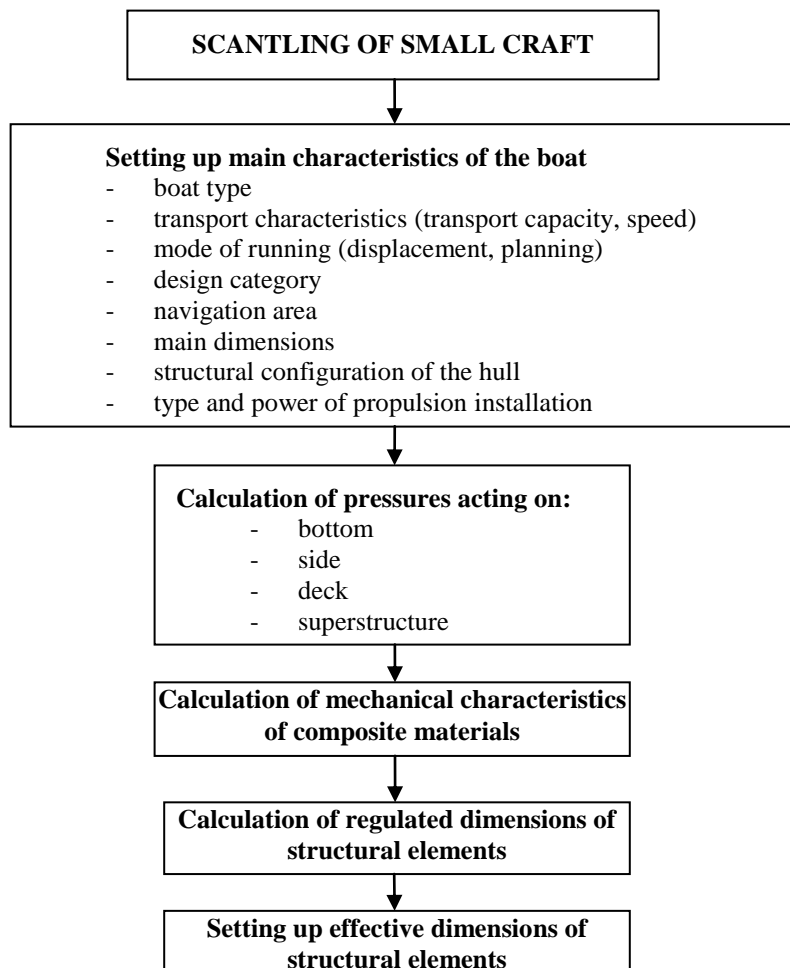


Figure 2: Scheme of boat scantling

Figure 3 presents the results of some comparative scantling calculations for boats made of composite materials according to the Rules of some classification societies and according to ISO 12215-5 : 2008, reproduced from [3]. We can conclude that boats dimensioned according to this standard are lighter than those dimensioned according to the Rules of main classification societies (LR, ABS, GL, BV or RINA).

Scantling of structural elements subject to concentrated loads could be performed through direct calculations, including finite element method.

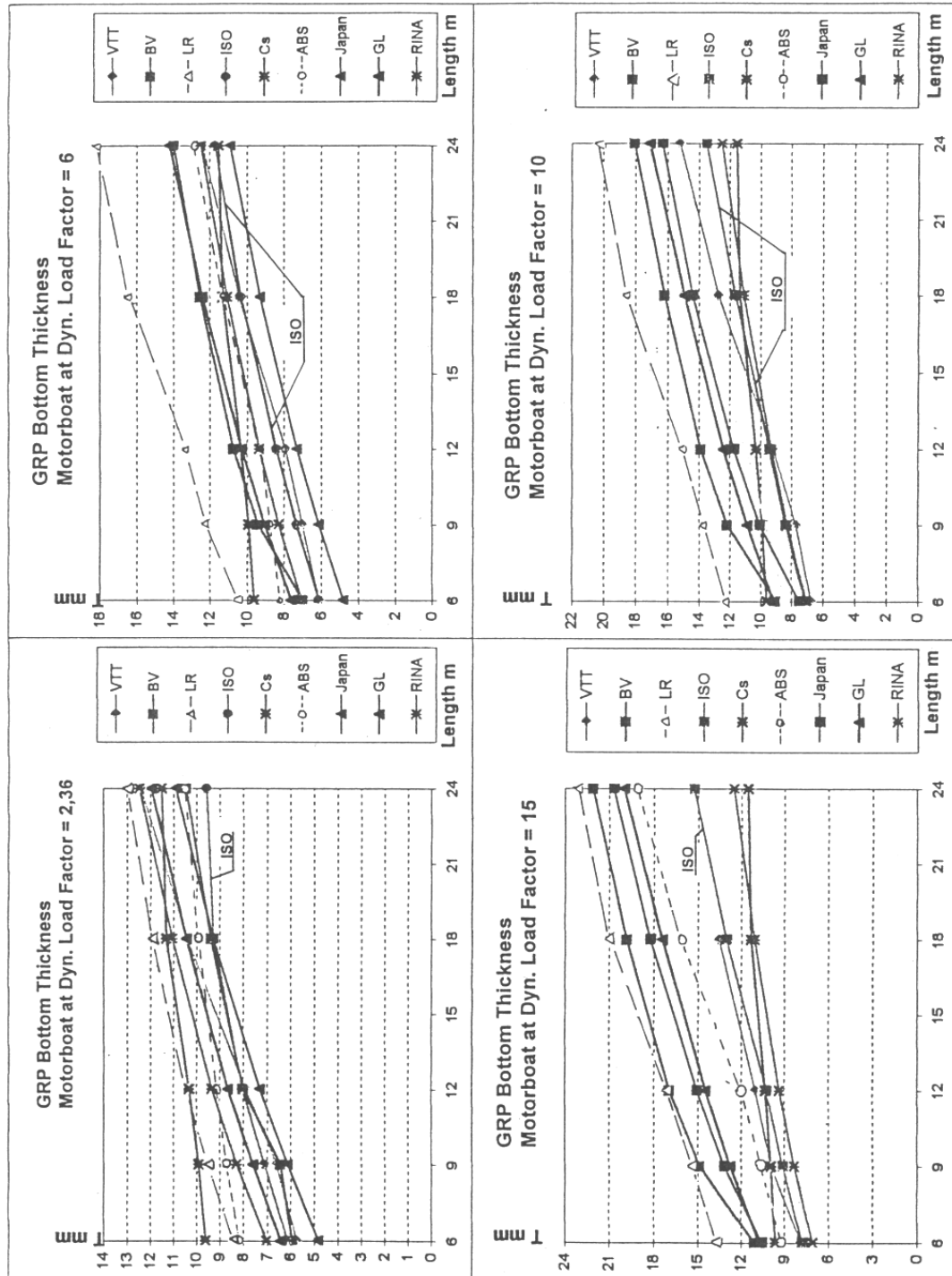


Figure 3: Comparative calculations for small craft scantlings

3. SCANTLING CALCULATIONS FOR A BOAT BASED ON INTERNATIONAL STANDARD ISO 12215-5:2008 USING CRAFTSOFT SOFTWARE

Based on standard ISO 12215-5 : 2008, a leisure boat in serial production was dimensioned, in order to fulfill essential requirements of Directive 94/25/EC, see figure 4. The characteristics of this boat are given in table 1.

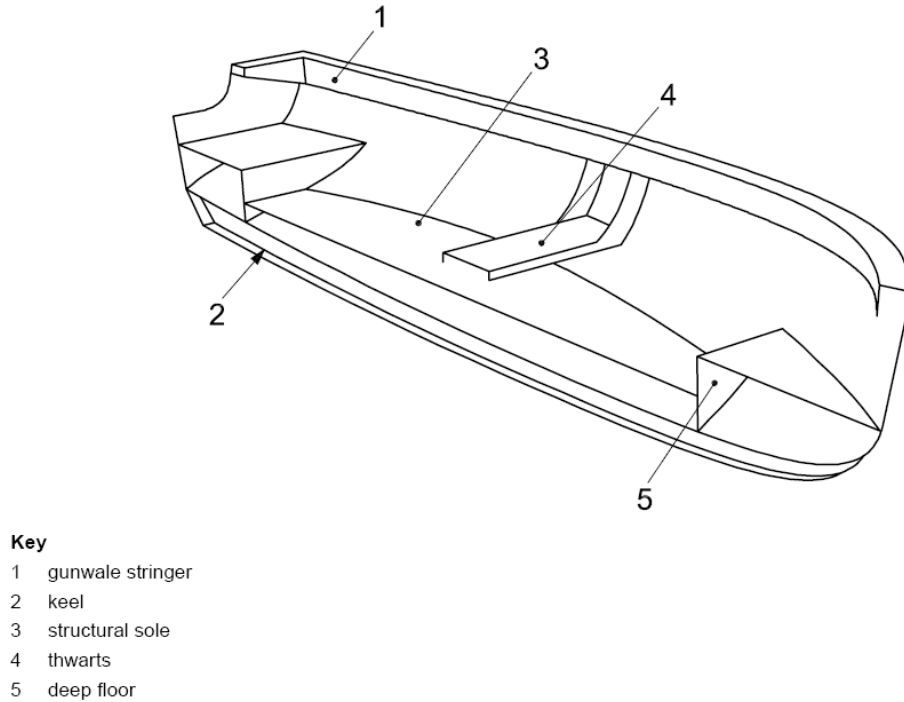


Figure 4: Structural arrangement of dimensioned boat

Table 1: Boat particulars

| | |
|-----------------------------------|---|
| Craft Type | Motor boat MFS-MB3 |
| Design Category | D |
| Material | GRP single-skin laminates and GRP sandwich composites |
| Displacement, m_{LDC} | 625.00 kg |
| Length of Hull, L_H | 4.50 m |
| Hull Beam, B_H | 1.40 m |
| Loaded Waterline Length, L_{WL} | 4.00 m |
| Loaded Waterline Beam, B_{WL} | 1.30 m |
| Chine Beam, B_C | 1.20 m |
| Depth of Bulkhead, D_b | 0.53 m |
| Deadrise Angle, $b_{0,4}$ | 17.00 ° |
| Maximum speed, V | 9.50 kts |

Because scantling calculations based on relevant ISO standard, are laborious and complex, a software named CraftSoft was developed in Excel. With its help, following calculations for structural elements of respective boat were performed, as indicated in the tables hereinafter:

Table 2: General calculation

| | |
|--|--------------------------|
| Dynamic Load Factor, n_{CG} | 0.916 |
| Design Category Factor, k_{DC} | 0.400 |
| Base Bottom Displacement Pressure, $P_{BMD\ BASE}$ | 40.084 kN/m ² |
| Base Bottom Planning Pressure, $P_{BMP\ BASE}$ | 20.567 kN/m ² |
| Minimum Bottom Pressure, $P_{BM\ MIN}$ | 5.279 kN/m ² |
| Minimum Side Pressure, $P_{SM\ MIN}$ | 1.440 kN/m ² |
| Base Deck Pressure, $P_{DM\ BASE}$ | 16.000 kN/m ² |
| Minimum Deck Pressure, $P_{DM\ MIN}$ | 5.000 kN/m ² |

Table 3: GRP laminates properties for single-skin panels and stiffeners

| | | |
|---|--|----------------------------|
| Fabrication procedures | Hand-laminated combined chopped strand mat (CSM)/woven roving (WR) | |
| Composite Evaluation Level | | EL-c |
| Multiplied factor, K_M | | 0.800 |
| Glass content in mass, ψ | | 0.250 |
| Ultimate tensile strength, σ_{ut} | | 53.600 N/mm ² |
| Ultimate compressive strength, σ_{uc} | | 87.600 N/mm ² |
| Ultimate flexural strength, σ_{uf} | | 110.700 N/mm ² |
| Ultimate in-plane shear strength, τ_u | | 46.400 N/mm ² |
| Interlaminar (out of plane) shear strength, $\tau_{u\ inter}$ | | 14.500 N/mm ² |
| In-plane modulus, E | | 3600.000 N/mm ² |
| In-plane shear modulus, G | | 2132.000 N/mm ² |

Table 4: GRP sandwich properties for transom panel

| | | |
|---|--|-----------------------------|
| Fabrication procedures | Wood core covered by an outer GRP laminate and an inner GRP laminate | |
| Wood core properties of sandwich | | |
| Wood type | | Fir |
| Wood density, ρ_c | | 0.470 kg/m ³ |
| Ultimate tensile strength, σ_{ut} | | 80.000 N/mm ² |
| Ultimate compressive strength, σ_{uc} | | 40.000 N/mm ² |
| Ultimate flexural strength, σ_{uf} | | 68.000 N/mm ² |
| Ultimate transverse shear strength, τ_u | | 10.000 N/mm ² |
| Young's modulus parallel to fibres, E_L | | 10000.000 N/mm ² |
| Young's modulus perpendicular to fibres, E_T | | 800.000 N/mm ² |
| Shear modulus, G | | 600.000 N/mm ² |
| Transverse contraction, μ_{TL} | | 0.330 |
| Outer and inner GRP laminates properties of sandwich | | |
| Composity Evaluation Level of laminates | | EL-c |
| Multiplied factor for laminates, K_M | | 0.800 |
| Glass content in mass of laminates, ψ | | 0.250 |
| Ultimate tensile strength, σ_{ut} | | 53.600 N/mm ² |
| Ultimate compressive strength, σ_{uc} | | 87.600 N/mm ² |
| Ultimate flexural strength, σ_{uf} | | 110.700 N/mm ² |
| Ultimate in-plane shear strength, τ_u | | 46.400 N/mm ² |
| Interlaminar (out of plane) shear strength, $\tau_{u\ inter}$ | | 14.500 N/mm ² |
| In-plane modulus, E | | 3600.000 N/mm ² |
| In-plane shear modulus, G | | 2132.000 N/mm ² |

Table 5: GRP single-skin panel geometry

| Item | Dimension and Location | | | | | | | |
|--------------|------------------------|-----------------|---------------------|-----------------------|----------|----------|----------|-----------|
| | Length l [mm] | Width b [mm] | Aspect Ratio l/b | Longit. pos. x [m] | Location | z [m] | h [m] | c [mm] |
| Bottom Panel | 2700 | 1400 | 1.929 | 2.500 | Bottom | - | - | 530 |
| Side Panel | 2700 | 1400 | 1.929 | 2.500 | Side | 0.230 | 0.115 | 530 |

Table 6: GRP single-skin panel calculations & results

| Item | Calculations to ISO 12215-5 standard | | | | | | | | | |
|--------------|--------------------------------------|----------|-------|-------|-------|-------|---------------------------|-----------|-------------------|-----------------------|
| | k_L | k_{AR} | k_2 | k_3 | k_C | k_z | P [kN/m ²] | t [mm] | t_{min} [mm] | $t_{adopted}$ [mm] |
| Bottom Panel | 1.000 | 0.250 | 0.495 | 0.028 | 0.500 | - | 5.279 | 4.81 | 3.81 | 5.00 |
| Side Panel | 1.000 | 0.250 | 0.495 | 0.028 | 0.500 | 0.5 | 2.804 | 3.50 | 3.81 | 5.00 |

Table 7: GRP sandwich panel geometry

| Item | Dimension and Location | | | | | | | |
|--------------|------------------------|-----------------|---------------------|-----------------------|----------|----------|----------|---------------------|
| | Length l [mm] | Width b [mm] | Aspect Ratio l/b | Longit. pos. x [m] | Location | z [m] | h [m] | Curvature c [mm] |
| Trasom Panel | 920 | 300 | 3.067 | 0.000 | Trasom | 0.300 | 0.150 | 0.000 |

Table 8: GRP sandwich panel calculations

| Item | Calculations to ISO 12215-5 standard | | | | | | | | | |
|--------------|--------------------------------------|----------|-------|-------|-------|-----------|-------|---------------------------|-----------------|-----------------|
| | k_L | k_{AR} | k_2 | k_3 | k_C | k_{KSH} | k_z | P [kN/m ²] | M_d Nmm/mm | F_d [N/mm] |
| Trasom Panel | 0.501 | 0.579 | 0.489 | 0.028 | 1.000 | 0.485 | 0.5 | 3.256 | 23.8563 | 0.4737 |

Table 9: GRP sandwich panel results

| Item | Required | | | | | | Adopted | | | | | | |
|--------------|----------------------------|---------------------------------|---------------------------------|--------------------|--------------------|---------------|---------------|---------------|---------------|---------------|----------------------------|---------------------------------|---------------------------------|
| | I [cm ⁴ /cm] | SM_o [cm ³ /cm] | SM_i [cm ³ /cm] | t_{omin} [mm] | t_{imin} [mm] | t_s [mm] | t_c [mm] | t_o [mm] | t_i [mm] | t_s [mm] | I [cm ⁴ /cm] | SM_o [cm ³ /cm] | SM_i [cm ³ /cm] |
| Trasom Panel | 0.00335 | 0.0089 | 0.00545 | 0.57 | 0.40 | 0.095 | 43.0 | 5.2 | 1.8 | 50 | 2.903 | 1.994 | 0.819 |

Table 10: Minimum sandwich skin fibre mass

| Item | Required | | | | | Adopted | | |
|--------------|----------|-------|-------|----------------------------------|----------------------------------|----------------------------------|----------------------------------|--|
| | k_4 | k_5 | k_6 | w_{os} [kg/m ²] | w_{is} [kg/m ²] | w_{os} [kg/m ²] | w_{is} [kg/m ²] | |
| Trasom Panel | 0.900 | 1.000 | 1.000 | 0.198 | 0.139 | 1.799 | 0.623 | |

Table 11: GRP stiffner geometry

| Item | Dimension and Location | | | | | | |
|------------------|------------------------|-------------------|-----------------------|----------|----------|----------|-------------------------|
| | Length l_u [mm] | Spacing s [mm] | Longit. pos. x [m] | Location | z [m] | h [m] | Curvature c_u [mm] |
| Keel | 2700 | 600 | 2.500 | Bottom | - | - | 0 |
| Gunwale stringer | 2700 | 500 | 2.500 | Side | 0.230 | 0.230 | 475 |

Table 12: GRP single-skin panel calculations & results

| Label | Calculations to ISO 12215-5 standard | | | | | | | | Required | | | Adopted | | |
|------------------|--------------------------------------|----------|-------|----------|----------|---------------------------|---------------|--------------|-----------------------------|--------------------------|-------------------------|-----------------------------|--------------------------|-------------------------|
| | k_L | k_{AR} | k_z | k_{CS} | k_{SA} | P [kN/m ²] | M_d [Nm] | F_d [N] | A_w [cm ²] | SM [cm ³] | I [cm ⁴] | A_w [cm ²] | SM [cm ³] | I [cm ⁴] |
| Keel | 1.0 | 0.25 | - | 1.000 | 5.000 | 5.279 | 1924.2 | 4276.1 | 1.843 | 71.798 | 90.056 | 3.500 | 76.32 | 1100.0 |
| Gunwale stringer | 1.0 | 0.25 | 0.0 | 0.514 | 7.500 | 1.600 | 249.9 | 1080.0 | 0.698 | 9.324 | 8.386 | 3.000 | 10.04 | 34.38 |

From the boats dimensioned this way, and being in use, we did not received complaints, which means that their design and construction were correct.

REFERENCES

- [1] Chirica I., Beznea E. F., Elasticity of anizotrop materials, Ed. Fund. Univ. Dunărea de Jos, Galați, 2004;
- [2] Det Norske Veritas, Classification notes no. 30.11 - Steel sandwich panel construction, 2012;
- [3] Hartz F., The Development of Scantling Requirements in Support of the European Boat Directive, The International HISWA Symposium on Yacht Design and Yacht Construction, 2005;
- [4] International Organization for Standardization, ISO 12205 – Part5. Small craft. Hull construction and scantlings. Design pressures for monohulls, design stresses, scantlings determination, 2008;
- [5] Lloyd's Register, Rules and Regulations for Classification of ships, 2014.